

# TWO NON-IDENTICAL UNIT SYSTEM WITH FAILURES DUE TO MECHANICAL FAULT AND RANDOM SHOCKS

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**Abstract—** The present paper deals with the analysis of a two unit redundant system in which both the units are dissimilar. Here the units can fail due to mechanical fault as well as due to random shocks.

Using regenerative point technique with Markov renewal process, various reliability characteristics of interest are obtained..

**Index Terms—** Random Shocks, Sojourn Time.

## I. INTRODUCTION

Several authors including [1,4,5] working in the field of reliability have analysed many engineering systems with the assumption that all the units of the system are of similar type. But there exists some two unit standby systems in which both the units are dissimilar with different costs and operating conditions.

Keeping the above view, we in this chapter analysed a two unit redundant system in which both the units are dissimilar. Here the units can fail due to mechanical fault as well as due to random shocks.

Using regenerative point technique with Markov renewal process, the following reliability characteristics of interest are obtained.

- (1) Transition and steady state transition probabilities
- (2) Mean Sojourn times in various states
- (3) Mean time to system failure (MTSF)

## II. MODEL DESCRIPTION AND ASSUMPTIONS

- A. The system consists of only two non-identical units in which first is operative and the second unit is kept as cold standby.
- B. First unit can sustain almost two shocks i.e. if the unit does not fail in first shock then it will definitely fail in the second shock. Also it can fail directly due to mechanical fault.
- C. Second unit can fail due to mechanical fault as well as due to random shocks and it cannot sustain more than one random shock.
- D. A single repair facility is considered in the system.
- E. Second unit is repairable if it is failed due to mechanical fault otherwise in case of random shocks send it for replacement.
- F. The priority in repair and replacement is given to the second unit over first unit.

*All the failure time distributions are assumed to be negative exponential while the distribution of repair and replacement time are arbitrary.*

## III. NOTATION AND SYMBOLS

$N_O$	:	Normal unit kept as operative
$N_S$	:	Normal unit kept as cold standby
$N_{O1}$	:	Normal unit as operative after observing first random shock
$F_r$	:	Failed unit under repair
$F_{wr}$	:	Failed unit waiting for repair
$F_{rep}$	:	Failed unit under replacement
$\alpha$	:	Constant rate of occurring first random shock to the first unit
$\beta$	:	Constant rate of occurring second random shock to the first unit
$\gamma$	:	Constant failure rate of first unit failed due to mechanical fault

$\delta$  : Constant failure rate of second unit failed due to random shock

$\lambda$  : Constant failure rate of second unit failed due to mechanical fault

$f(\cdot), F(\cdot)$  : pdf and cdf of time to repair of first unit

$g(\cdot), G(\cdot)$  : pdf and cdf of time to replacement of second unit failed due to random shock

$h(\cdot), H(\cdot)$  : pdf and cdf of time to repair of second unit failed due to mechanical fault

Using the above notation and symbols the possible states of the system are

#### Up States

$S_0 \equiv (N_O, N_S)$   $S_1 \equiv (N_{O1}, N_S)$

$S_2 \equiv (F_r, N_O)$

#### Down States

$S_3 \equiv (F_{wr}, F_{rep})$   $S_4 \equiv (F_{wr}, F_r)$

The possible transitions between the states for analysis the above model are

$S_0 \rightarrow S_1, S_0 \rightarrow S_2, S_1 \rightarrow S_2, S_2 \rightarrow S_0, S_2 \rightarrow S_3, S_2 \rightarrow S_4, S_3 \rightarrow S_2$

$S_4 \rightarrow S_2$

#### IV. TRANSITION PROBABILITIES

Let  $T_0 (=0), T_1, T_2, \dots$  be the epochs at which the system enters the states  $S_i \in E$ . Let  $X_n$  denotes the state entered at epoch  $T_{n+1}$  i.e. just after the transition of  $T_n$ . Then  $\{T_n, X_n\}$  constitutes a Markov-renewal process with state space  $E$  and

$Q_{ik}(t) = \Pr[X_{n+1} = S_k, T_{n+1} - T_n \leq t | X_n = S_i]$   
....(1)

is semi Markov-Kernal over  $E$ . The stochastic matrix of the embedded Markov chain is

$P = p_{ik} = \lim_{t \rightarrow \infty} Q_{ik}(t) = Q(\infty)$   
....(2)

Thus, we get

$$p_{01} = \frac{\alpha}{\alpha + \gamma}$$

$$p_{02} = \frac{\gamma}{\alpha + \gamma}$$

$$p_{12} = 1$$

$$p_{20} = f^*(\delta + \lambda)$$

$$p_{23} = \frac{\delta}{\delta + \lambda} [1 - f^*(\delta + \lambda)]$$

$$p_{23} = \frac{\lambda}{\delta + \lambda} [1 - f^*(\delta + \lambda)]$$

$$p_{32} = 1$$

$$p_{42} = 1$$

....(3-10)

From the above probabilities the following relations can be easily verified as;

$$p_{01} + p_{02} = 1 = p_{12} = p_{32} = p_{42}$$

$$p_{20} + p_{23} + p_{24} = 1$$

....(11-12)

#### V. MEAN SOJOURN TIMES

The mean time taken by the system in a particular state  $S_i$  before transiting to any other state is known as mean sojourn time and is defined as

$$\mu_i = \int_0^\infty P[T > t] dt$$

....(13)

Where  $T$  is the time of stay in state  $S_i$  by the system.

To calculate mean sojourn time  $\mu_i$  in state  $S_i$ , we assume that so long as the system is in state  $S_i$ , it will not transit to any other state. Therefore;

$$\mu_0 = \int_0^\infty e^{-(\alpha + \gamma)t} dt = \frac{1}{\alpha + \gamma}$$

$$\mu_1 = \int_0^\infty e^{-\beta t} dt = \frac{1}{\beta}$$

$$\mu_2 = \int_0^\infty e^{-(\delta + \lambda)t} \bar{F}(t) dt = \frac{1}{\delta + \lambda} [1 - f^*(\delta + \lambda)]$$

$$\mu_3 = \int_0^\infty \bar{G}(t) dt = \int_0^\infty t.g(t) dt$$

$$\mu_4 = \int_0^\infty \bar{H}(t) dt = \int_0^\infty t.h(t) dt$$

....(14-18)

#### Contribution to Mean Sojourn Time

For the contribution to mean sojourn time in state  $S_i \in E$  and non-regenerative state occurs, before transiting to  $S_j \in E$ , i.e.,

$$m_{ij} = - \int_0^\infty t.q_{ij}(t) dt = -q'^*_{ij}(0)$$

....(19)

Therefore,

$$m_{01} = \int_0^\infty \alpha.t.e^{-(\alpha + \gamma)t} dt = \frac{\alpha}{(\alpha + \gamma)^2}$$

$$m_{02} = \int_0^\infty \gamma \cdot t \cdot e^{-(\alpha+\gamma)t} dt = \frac{\gamma}{(\alpha + \gamma)^2}$$

$$m_{12} = \int_0^\infty \beta \cdot t \cdot e^{-\beta t} dt = \frac{1}{\beta}$$

$$m_{20} = \int_0^\infty t \cdot e^{-(\delta+\lambda)t} f(t) dt$$

$$m_{23} = \delta \cdot \int_0^\infty t \cdot e^{-(\delta+\lambda)t} \bar{F}(t) dt$$

$$m_{24} = \lambda \cdot \int_0^\infty t \cdot e^{-(\delta+\lambda)t} \bar{F}(t) dt$$

$$m_{32} = \int_0^\infty t \cdot g(t) dt$$

$$m_{42} = \int_0^\infty t \cdot h(t) dt$$

....(20-27)

Hence

$$m_{01} + m_{02} = \frac{1}{\alpha + \gamma} = \mu_0$$

$$m_{12} = \frac{1}{\beta} = \mu_1$$

$$m_{20} + m_{23} + m_{24} = \frac{1}{\delta + \lambda} [1 - f^*(\delta + \lambda)] = \mu_2$$

$$m_{32} = \int_0^\infty t \cdot g(t) dt = \mu_3$$

$$m_{42} = \int_0^\infty t \cdot h(t) dt = \mu_4$$

....(28-32)

## VI. MEAN TIME TO SYSTEM FAILURE (MTSF)

To obtain the distribution function  $\pi_i(t)$  of the time to system failure with starting state  $S_0$ .

$$\pi_0(t) = Q_{01}(t) \pi_1(t) + Q_{02}(t) \pi_2(t)$$

$$\pi_1(t) = Q_{12}(t) \pi_2(t)$$

$$\pi_2(t) = Q_{20}(t) \pi_0(t) + Q_{23}(t) + Q_{24}(t) \quad \dots(.33-35)$$

Taking Laplace Stieltjes transform of relations (33-35)

and solving them for  $\tilde{\pi}_0(s)$  by omitting the argument 's' for brevity, one gets

$$\tilde{\pi}_0(s) = N_1(s) / D_1(s) \quad \dots(36)$$

where

$$N_1(s) = \tilde{Q}_{01} \tilde{Q}_{12} \tilde{Q}_{23} + \tilde{Q}_{01} \tilde{Q}_{12} \tilde{Q}_{24} + \tilde{Q}_{02} \tilde{Q}_{23} + \tilde{Q}_{02} \tilde{Q}_{24} \quad \dots(37)$$

and

$$D_1(s) = 1 - \tilde{Q}_{01} \tilde{Q}_{12} \tilde{Q}_{20} - \tilde{Q}_{02} \tilde{Q}_{20} \quad \dots(38)$$

The mean time to system failure (MTSF) when the system starts from  $S_0$  is

$$E(T) = - \frac{d}{ds} \pi_0(s) |_{s=0} = \frac{D'_1(0) - N'_1(0)}{D_1(0)} \quad \dots(39)$$

where

$$N_1 = \mu_0 + \mu_1 p_{01} + \mu_2 \quad \dots(40)$$

and

$$D_1 = 1 - p_{20} \quad \dots(41)$$

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